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Antenna Suspects

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Updated article version

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Introduction

url: http://www.radiohamtech.com/page27.html
url: http://www.radiohamtech.com/page20.html

First thought, we start by asking the question, “what is the inductance of one metre of wire”, fair question, but how does one find out so.

The trick here is to use the equation for the “characteristic impedance of a transmission line”, namely:-

Cable impedance = SQR(inductance / capacitance)

We know that the impedance is 50ohms, and the capacitance per metre is 100pF / m, ‘RG58C/U’, the inductance per metre calculates out as :

50^2 * 100pF = 250nH / metre

The next question, as the wire is one metre in length, and the full wavelength of 300MHz is one metre, what is then the inductive reactance to the one metre wire to a 300MHz carrier.

Inductive reactance = 2 * PI * F * inductance

XL = 2 * PI * 300MHz * 250nH

XL = 471 ohms

If the full wave antenna induces into it a 5 Volt EMF signal, then what is the RF signal power.

The contents worded here, is my own handy work. To date I have not found any other periodical that has shown anything similar towards these contents, contained within this article type booklet.

The calculation methodology shown here, of antenna designs, is through my own understandings.

RF signal power

Our next question is how to do calculate the RF signal power induced into an antenna.

This can be achieved by measuring the voltage across the antenna load.

power = voltage ^2 / resistance

But first, how do you prove the power equation is correct.

An alternative power equation is :- power = volts * current

First consider “ohms Law”, which equates to as :- Volts = current * resistance

However, measuring current in an RF signal is not so easy. By using “ohms Law”, the current component can be replaced as follows:

Current = volts / resistance

Now place this into the equation :- power = volts * current,

The following results : power = volts * (volts / resistance)

When the above equation is merged, the following given equation is

power = (volts * volts) / resistance

Looking back at our full wave antenna, the RF signal of the induced 5 Volts can thus be calculated.

power = (5 * 5) / 50

power = ½ Watts, or 0·5 Watts

Using this above equation, the RF signal power can be calculated by just measuring the RF voltage and with a known terminal impedance of the RF loading, namely the Radio itself.

In order to determine the effectiveness of an antenna design, this article compares several antenna methods to a full wavelength antenna transmission or reception.

Stub Antenna's

Now this is fine so far, but then a 50ohm stub antenna would have a 50ohm inductive reactance, if so, then what is the length of a 50ohm stub at 300MHz.

Remember, referencing to the full wave wire antenna impedance of 565 ohms, also there are 100cm in one metre length.

Thus, to find out :- (50 / 471) * 100cm = 10·6cm

Now the 10·6cm long in length 50ohm stub antenna, what is the signal pick up, when compared to a full wavelength one metre 300MHz long wire, however it need not be a 300MHZ example shown here.

It could instead be 30MHz or the 10m band, thus then the 50ohm stub for the 10m band is 106cm. For the 2m band, then the length is 21·9cm (145MHz) for the 50ohm stub, while for the 70cm band, the 50ohm stub antenna is 7·3cm (435MHz) in length.

It may be perhaps that a smaller wire would pick up (or induce) a lesser signal, where as a longer wire may receive (or induce) a bigger signal, from the etha signal, the etha signal the induction voltage from electromagnetic field strength of the radio signal within the air, i.e. the etha.

Assuming that full wave 471ohm impedance is matched to a 50ohm load, then the induced RF voltage into the full wave antenna is 5 volts would be presented to the radio terminal input.

However, how much of the RF signal is induced into or from an 50ohm stub antenna, that is now only 10·6% of the length of the original full wave antenna wire or element.

By the same principle, the 50ohm stub received signal is :

(50/471) * 5 = 530mV

The 50ohm stub antenna as one can see here in this example, only picks up or send out 443mV of the signal, too and from the “etha” (the surrounding air). Remember, what happens to a Rx antenna, happens to an Tx antenna.

The 50ohm stub signal power equates to:

power = (530mV * 530mV) / 50

power = 5·6mW

The equate the 50ohm stub antenna design into suspect numbers, using “LOG to the base of ten”,

dB = 10 * Log(5·6mW / 0·5 Watt)

dB = -19·5

Now perhaps an idea to improve the 50ohm stub antenna design, would be to double up on the stub antenna design, say two 50ohm stubs, one on top of the other in a line.

The 50ohm stub antenna would thus become a 100ohm stub antenna, a double side stub antenna, what would this give us Radio Hams if a 100ohm stub design were used for an antenna with our radios.

By the same principle, the 100ohm stub received signal is :

(100/471) * 5 = 1V

The 100ohm stub signal power equates to:

power = (1V * 1V) / 50

power = 20mW

The equate the 100ohm stub antenna design signal performance:

dB = 10 * Log(20mW / 0·5 Watt)

dB = -13·9 dB, or a 13·9 dB loss

Half wave dipole

A half wave dipole is made from two quarter wave sections. A full wave wire is 565ohms, so a quarter wave section would be :

quarter wave section “XL” = 471 /4 = 117·75 ohms

As each radiating element on each side of a coax, as a dipole would be, is effectively in parallel.

If both quarter wave sections where attached to a coax, then each side would be 141ohms. The coax would then see:

coax load = 117·75 / 2 = 58 ohms,

Which would then equate to the 58ohms (or 75ohms) the books say.

For a 50ohm coax load, each side of the dipole would need to 100ohms.

Now the true quarter wave is 117·75ohms, so the trim for a 50ohm dipole quarter wave would then be as such:

50ohm dipole quarter wave trim to length = 100 / 117·75 = 85% overall.

The knocking off 5%, just became a 15% trim off the true quarter wave wire.

As it happens, a 50ohm dipole each side has an inductive reactance of 100 ohms for each dipole element, which seems to equate two 50ohm stub antennas on top of each other.

As each side of the 50ohm dipole is 100ohms, the total inductive reactance is 200ohms, both sides added together.

Well things work as such, by the following:

signal pickup of the 50ohm dipole = (200 / 471) * 5 = 2·1Volts.

Now convert this into signal power of Watts, remember power = V^2 / R

thus, the power dipole (50ohms) = (2·1 * 2·1) / 50 = 88mW

dB gain = 10 *Log (88mW / 0.5 Watts)

dB gain = -7·5dB, or a 7·5dB loss

Now for a 50ohms cross dipole, each side element is 200ohms, thus each has two 200ohms elements positioned sideways in a “V” shape, effectively with each side a “V” shape antenna element, equalling out to 100ohms load.

As each side of the “V” shape element has two 200ohms elements, equating with both sides to any overall 4 elements, each of 200 ohms, this then totals to an overall 800ohms inductive reactance used for the cross-dipole design.

Signal pickup of a cross 50ohm dipole = (800 / 471) * 5 = 8·5Volts.

Thus, the RF signal power from the 50ohm cross dipole design:

power = (8·5 * 8·5) / 50 = 1·4 Watts

dB gain = 10 *Log (1·4 Watts / 0·5 Watts)

dB gain = 4·5dB for a cross element dipole

Between the standard 50ohm dipole and the 50ohm cross dipole, there is a 12dB difference.

Now this bit of the article booklet is just theoretical, but, if your beam has a 10·5dB gain over a dipole, with the dipole 7·5dB calculation loss, the beam could be a 3dBm gain over a full wave vertical or wire.

Replace the 50ohm dipole with a 50ohm cross dipole, the beam of a 10·5dB over a dipole, despite the dipole losses, would then be a 10·5dB + 4·5dB “cross dipole”, equating to a near 15dB gain over a full wave vertical, as an emf voltage within the etha.

Equates as : 10^(15/10) = 31 times power improvement of concentrated signal, or as a signal voltage improvement, 10^(15/20) = 5·6 times voltage :

equates to as V^2/R = (5.6 * 5.6) / 1 = 31 times.

(the “1” is a normalised magnitude value of 50hms)

In essence, a 15dB signal improvement upon the receiver input from the antenna, or a near 2 - 3 “S points” improvement.

One could try swapping their 50ohm dipole on their beam antenna for a 50ohm cross dipole version

To be sure to here, one must go by one’s own experience regarding beam antennas.

Antenna inductance

You may perhaps remember from the start of the article, that the length of a one metre was around the 300nH mark, or 0·3uH overall.

To calculate the antenna elements inductance, follow the below example.

The length of the 10m 50ohm stub was 106cm, also there are 100cm to one metre of wire antenna.

therefore, the inductance of the 10m 50ohm stub antenna is:

(106 / 100) * 250nH = 265nH or 0·265uH

Now if one is building one's own 10m “walkie talkie”, then replace the 106cm wire whip for a 265nH inductor.

Now the thought of how this, is a fair question, monitoring the bands I have noticed some asking the same question to fellow hams. The best answer I can offer, is the following.

The antenna radiation, of the current lobe, is compressed into the length of the coiled 265nH inductor, instead of the radiation current being spread over the 106cm antenna whip.

As the inductor is a compressed magnetic field in any case, this may well be the answer to why I think that the inductor sized 50ohm stub antenna would still function, being in mind that the 106cm wire whip, is a long wire inductor.

Dipole antenna load coils for 80m / 40m band operation.

Now here is one trick to think off.

If one were to replace the dipole elements with an inductor, what would occur.

Should one wish to construct an 80m dipole, each side would then be 14·2m in length, or 28·4m overall, or a 4·2uH of inductance for each side element of the dipole, remembering that the inductive reactance of each element of a 50ohm dipole equals 100ohms:

$$(100 / 471) * 80m * 0{\cdot}25uH/m = 4{\cdot}2uH$$

For the 80m band 50ohm dipole, each element equates to 4·2uH in value.

If the loft has only 6metres of space to hand, then replacing some of the dipole wire with an inductance would be helpful.

Reducing the 17m dipole element to just 1·7m would be nice to do. The load inductance for the dipole displacement coils, could then be calculated.

Load coil inductance, (displacement coil)

$$17m – 1{\cdot}7m = 15{\cdot}3m$$

Which then calculates the load coil inductance to as:

$$15{\cdot}3m * 250nH$$

Load coil inductance = 3·825uH, or 3·8uH to round up.

By placing the load coil on both sides of the 80m dipole, the overall length of the 80m dipole could be kept down to 3·4m overall, to fit a 6m length loft area.

An interesting thought though, a switching relay circuit system could be used to switch from the 80m (3·8uH load coil) to the 40m band (6·7uH load coil), for each side of dipole using the 1·7m element length, together with the band switched inductance loading coils.

300ohm coax Dipole

Likewise, if the design is for a 300ohm ribbon cable dipole, then each side of the 300ohm dipole would be 600ohms, for the very same reasons, in other words, each radiating element of a dipole antenna, would be 600ohm inductive reactance.

600 / 471 = 127%,

The induced RF signal voltage would just 27% greater than a full wave antenna wire, but also the dimensions of 300ohm coax dipole, each side is also 27% greater than a full wave wire antenna.

However, as each side is 600 ohms, the total inductive reactance used is 600 * 2 = 1200 ohms

The antenna performance equates to as :

(1200 / 471) * 5 = 12·7 Volts

power = (12·7 * 12·7) / 50

power = 3·2 Watts

Completing the antenna performance calculation:

dB gain = 10 *Log (3·2 Watts / 0·5 Watts)

dB gain = 8dB overall

This means that a 300ohm coax dipole has basically an 8dB advantage over a full wave long wire antenna. For a 100Watt transmitter, this is 630 Watts, or there about and 8dBm increase in the receiver's sensitivity.

If should the dipole design be a **300ohm cross dipole design,** then each element section would be 1200 ohms. The overall total inductive reactance used for a 300ohm cross dipole, would be 4 * 1200 ohms, equating thus to 4800 ohms overall.

Effective change of accumulated induced RF signal voltage of a 300ohm ribbon cross dipole design:

4800 / 471 = 10·2 times greater

The induced voltage reference to the full wave 5 Volts, equates to :

(4800 / 471) * 5 = 51 Volts

The RF signal power of the 300ohm cross dipole reception is thus :

power = (51 * 51) / 50

power = 52 Watts

Completing the 300ohms cross dipole antenna performance calculation:

dB gain = 10 * Log (52Watts / 0·5 Watts)

dB gain = 20·2 dB overall

This equates also to a 20dB signal improvement upon the receiver, or a near ‘3 – 4’ “S point” improvement.

For a lumped component 300ohm coax dipole design, with each side of the dipole just an inductance coil, at an antenna boost of 8dB overall, or 6 times Tx power.

A 100 Watt Tx would seem as a 600 Watt Tx overall output.

Dipole : band wavelength * (600 / 471) * 250nH = load coil dipole lump element

160m dipole load coil element = 51uH

80m dipole load coil element = 25·5uH

60m dipole load coil element = 19uH

40m dipole load coil element = 12·7uH

17m dipole load coil element = 5·4uH

15m dipole load coil element = 4·8uH

12m dipole load coil element = 3·8uH

10m dipole load coil element = 3·2uH

6m dipole load coil element = 1·9uH

4m dipole load coil element = 1·3uH

With the feed point at 300ohms, then a 300ohm to 50ohm balun would be required to interface a 50ohm coax cable. For multi band use, remote switch the load coils.

For a 300ohm cross dipole, this equates to a 20dB or 100 times gain overall, a ‘3 – 4’ “S points” advantage, or a 20dB increase for the radio receiver signals range.

Cross : band wavelength * (1200 / 471) * 250nH = load coil dipole lump element

160m dipole load coil element = 101uH

80m dipole load coil element = 51uH

60m dipole load coil element = 38uH

40m dipole load coil element = 25·4uH

17m dipole load coil element = 10·8uH

15m dipole load coil element = 9·6uH

12m dipole load coil element = 7·6uH

10m dipole load coil element = 6·4uH

6m dipole load coil element = 3·8uH

4m dipole load coil element = 2·5uH

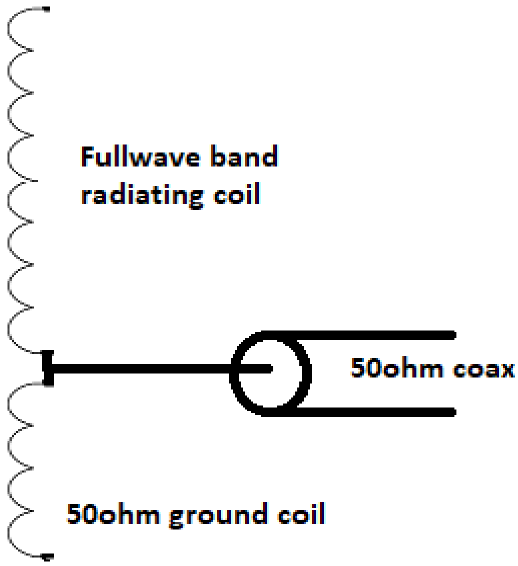
A 10Watt qrp radio with a 300ohm cross dipole, would seem as 1KW transmitter output.

A 100Watt radio, running as they say “bare foot”, with a 300ohm cross dipole, would seem as 10KW transmitter output.

Be careful as to the band plan ERP limits for your ham radio licence.

Lumped Component coiled vertical antenna

View the below diagram:



The top coil is used as the radiating element, inductance reactance of 565ohms, but may be a multiple of wavelengths of extra signal gain. The grounding coil is used to impedance match the radiating coil to the 50ohm coax, as well as the radio itself.

For the 80m band, the full wave load coil inductance :

80m * 0·25uH/m = 20uH "or 40uH for two wavelengths etc"

The 80m 50ohm ground loading coil inductance :

(50 / 471) * 80m = 8·5uH "remains a 80m band constant"

The principle here, the vertical antenna is full wavelength, thus the radiating coil would have a full electromagnetic connection to the surrounding etha. This based on the idea that a full wave would in thought have a purposeful "1:1" turns ratio connection to the etha.

However, the insertion loss between the antenna and the etha, is based on the idea of a weak "B/H" magnetic curve of the etha environment. The "B/H" curve losses, would be on top of any other propagation losses.

The antenna design is essentially an off-centred dipole, replacing a wire inductance radiating element, by coiled inductance radiating elements.

Hope folks, this helps.

Antenna Path Ratios

Much over the airwaves has been mentioned or talked about, relating to the benefits of one's own application of an antenna system.

Over the last few years, I have been attempting to derive a propagation program to at least try to un-tangle the physics behind just the "Inverse Square Law of signal decay", relative to the transmitter power output, the antenna system used, and the RF bandwidth of the receivers front end design.

I started the quest with a degree of log notes related to the local 70cm repeater, and then onto a HF contact some 3000Km away towards Europe. The QSO occurred on the 40m band, while using a bitx40 operating through a 40m wire via a 9:1 balam. The radio ham some 3000Km away, was using a dipole and a transmitter power output of some 350Watts. Please note also the front-end bandwidth change the radio receiver's performance, as relating to the radio in hand, the bitx40 and the QSO end.

I found that while developing the Inverse Square Law application, an additional factor variable had to be taken into the equations. The signal values recorded in my logbook, did not match the prediction, so an "additional signal path loss" was added. This then gave the ability to change the path loss variable for bad days and good days of a signal lift.

On the whole the "additional signal path loss" averages to a 70dB increase in signal path losses. Whether this changes from HF to Microwaves is unknown, but it did seem otherwise to be the insertion loss connection of the antenna system, between the two stations. The "Inverse Square Law" equation itself, did not go fully to explain the communications pathway physics figures.

The first image, page 14, relates to the bitx40 both sides, with the 40m wire antenna, obtaining a QSO distance of some 3000Km.

The second image, page 15, relates to a European return station, using a dipole, please note the transmitter power that was used to make the return path. This is some 350Watts to bridge the 3000Km distance. The third image, page 18, shows the transmitter requirements for a 50ohm stub antenna used by the European station, some 3000Km away. Do please note the return path transmitter prediction of some 4500Watts. Both cases assuming a front-end bandwidth of 4MHz

The fourth image, page 17, shows the bitx40 both sides using a 50ohm dipole. The effective QSO distance then drops down to some 375 miles maximum of distance, the contact also using a 50ohm dipole.

My own radio has a 4MHz front-end bandwidth on the 40m band, as I found most manufacturer radio do so, although I understand the bitx40 is a 500KHz bandwidth.

radio base to propagation distance.bbc

```
-104.397431dBW  = 42.62uV
-149.0309dBW = 0.25uV
-103.0103dBW  = 50uV
-151.189008dBW  = 0.195uV


Rx Radio noise figure = 4.8 dB
Rx Audio signal to noise = 10 dB
Rx test bw Bw = 2700 Hz
Radio base line = 0.25 uV

Radio front-end Bw = 0.5 MHz
Tx power watts = 7 Watts
Frequency of signal = 7 MHz

antenna radio 'Tx' set 1 = 100 % eff.   0     dB 'Tx antenna'
antenna radio 'Rx' set 2 = 100 % eff.   0     dB 'Rx antenna'

additional signal path loss dB = 70dB

Reach RF Tx budget watts = 700 nW
Reach RF Tx budget dBW   = -61.55 dBW
```

[------------- Radio set 2	-------------				------------------]	[------------- Radio set 1	-------------		------------------]
Rx signal	com's range		ERP Watts	EMF uV	EMF 'S'	Rx 'S'	Rx dBW	Rx uV	
-126.17 dBW	5803.7 Km	3627.3 miles	7	3.47	4.65	4.65	-126.17	3.47	10 dB s/n
-123.17 dBW	4110.1 Km	2568.8 miles	7	4.9	5.22	5.22	-123.17	4.91	13 dB s/n
-120.17 dBW	2909.7 Km	1818.6 miles	7	6.93	5.78	5.78	-120.17	6.93	16 dB s/n
-117.17 dBW	2059.9 Km	1287.4 miles	7	9.79	6.34	6.34	-117.17	9.79	19 dB s/n
-114.17 dBW	1458.3 Km	911.4 miles	7	13.83	6.9	6.9	-114.17	13.84	22 dB s/n
-111.17 dBW	1032.4 Km	645.2 miles	7	19.54	7.47	7.47	-111.17	19.54	25 dB s/n
-108.17 dBW	730.9 Km	456.8 miles	7	27.6	8.03	8.03	-108.17	27.61	28 dB s/n

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radio base to propagation distance.bbc

```
-104.397431dBW  = 42.62uV
-149.0309dBW = 0.25uV
-103.0103dBW  = 50uV
-151.189008dBW  = 0.195uV


 Rx Radio noise figure = 4.8 dB
 Rx Audio signal to noise = 10 dB
 Rx test bw Bw = 2700 Hz
 Radio base line = 0.25 uV

 Radio front-end Bw = 4 MHz
 Tx power watts = 350 Watts
 Frequency of signal = 7 MHz

 antenna radio 'Tx' set 1 = 35.39 % eff. -9.1  dB 'Tx antenna'
 antenna radio 'Rx' set 2 = 100 % eff.   0     dB 'Rx antenna'

 additional signal path loss dB = 70dB

 Reach RF Tx budget watts = 4305 nW
 Reach RF Tx budget dBW   = -53.66 dBW


   [-------------------------------- Comm's channel -----------------------------------]   [----------------- radio unit -----------------]

     Rx signal           com's range               ERP Watts      EMF uV        EMF 'S'        Rx 'S'    Rx dBW      Rx uV


    -117.14 dBW     5089.1 Km    3180.7 miles        43.05        9.82          6.35           6.35     -117.14      9.83       10 dB s/n

    -114.14 dBW     3604.5 Km    2252.8 miles        43.05        13.88         6.91           6.91     -114.14      13.88      13 dB s/n

    -111.14 dBW     2551.8 Km    1594.8 miles        43.05        19.61         7.47           7.47     -111.14      19.61      16 dB s/n

    -108.14 dBW     1806.5 Km    1129 miles          43.05        27.7          8.04           8.04     -108.14      27.71      19 dB s/n

    -105.14 dBW     1278.9 Km    799.3 miles         43.05        39.12         8.6            8.6      -105.14      39.14      22 dB s/n

    -102.14 dBW     905.4 Km     565.8 miles         43.05        55.26         9.16           9.16     -102.14      55.29      25 dB s/n

    -99.14 dBW      640.9 Km     400.6 miles         43.05        78.07         9.72           9.72     -99.14       78.1       28 dB s/n
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radio base to propagation distance.bbc

```
-104.397431dBW  = 42.62uV
-149.0309dBW = 0.25uV
-103.0103dBW  = 50uV
-151.189008dBW  = 0.195uV

 Rx Radio noise figure = 4.8 dB
 Rx Audio signal to noise = 10 dB
 Rx test bw Bw = 2700 Hz
 Radio base line = 0.25 uV

 Radio front-end Bw = 4 MHz
 Tx power watts = 4500 Watts
 Frequency of signal = 7 MHz

 antenna radio 'Tx' set 1 = 8.84 % eff.  -21.1 dB 'Tx antenna'
 antenna radio 'Rx' set 2 = 100 % eff.   0     dB 'Rx antenna'

 additional signal path loss dB = 70dB

 Reach RF Tx budget watts = 3493 nW
 Reach RF Tx budget dBW   = -54.57 dBW
```

[-------------------------------- Comm's channel ---------------------------------] [------------------ radio unit ------------------]

Rx signal	com's range		ERP Watts	EMF uV	EMF 'S'	Rx 'S'	Rx dBW	Rx uV	
-117.14 dBW	4583.7 Km	2864.8 miles	34.93	9.82	6.35	6.35	-117.14	9.83	10 dB s/n
-114.14 dBW	3246.5 Km	2029 miles	34.93	13.88	6.91	6.91	-114.14	13.88	13 dB s/n
-111.14 dBW	2298.3 Km	1436.4 miles	34.93	19.61	7.47	7.47	-111.14	19.61	16 dB s/n
-108.14 dBW	1627.1 Km	1016.9 miles	34.93	27.7	8.04	8.04	-108.14	27.71	19 dB s/n
-105.14 dBW	1151.9 Km	719.9 miles	34.93	39.12	8.6	8.6	-105.14	39.14	22 dB s/n
-102.14 dBW	815.4 Km	509.6 miles	34.93	55.26	9.16	9.16	-102.14	55.29	25 dB s/n
-99.14 dBW	577.3 Km	360.8 miles	34.93	78.07	9.72	9.72	-99.14	78.1	28 dB s/n

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radio base to propagation distance.bbc

```
-104.397431dBW  = 42.62uV
-149.0309dBW = 0.25uV
-103.0103dBW  = 50uV
-151.189008dBW  = 0.195uV

 Rx Radio noise figure = 4.8 dB
 Rx Audio signal to noise = 10 dB
 Rx test bw Bw = 2700 Hz
 Radio base line = 0.25 uV

 Radio front-end Bw = 0.5 MHz
 Tx power watts = 5 Watts
 Frequency of signal = 7 MHz

 antenna radio 'Tx' set 1 = 35.39 % eff. -9.1  dB 'Tx antenna'
 antenna radio 'Rx' set 2 = 35.39 % eff. -9.1  dB 'Rx antenna'

 additional signal path loss dB = 70dB

 Reach RF Tx budget watts = 61 nW
 Reach RF Tx budget dBW   = -72.12 dBW
```

[------ Comm's channel					------]	[------ radio unit			------]
Rx signal	com's range		ERP Watts	EMF uV	EMF 'S'	Rx 'S'	Rx dBW	Rx uV	
-117.07 dBW	603.4 Km	377.1 miles	0.61	9.9	6.36	4.65	-126.17	3.47	10 dB s/n
-114.07 dBW	427.3 Km	267.1 miles	0.61	13.99	6.92	5.22	-123.17	4.91	13 dB s/n
-111.07 dBW	302.5 Km	189 miles	0.61	19.76	7.49	5.78	-120.17	6.93	16 dB s/n
-108.07 dBW	214.1 Km	133.8 miles	0.61	27.92	8.05	6.34	-117.17	9.79	19 dB s/n
-105.07 dBW	151.6 Km	94.7 miles	0.61	39.44	8.61	6.9	-114.17	13.84	22 dB s/n
-102.07 dBW	107.3 Km	67 miles	0.61	55.71	9.18	7.47	-111.17	19.54	25 dB s/n
-99.07 dBW	75.9 Km	47.4 miles	0.61	78.7	9.74	8.03	-108.17	27.61	28 dB s/n

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